NORDIC AQUAFARMS
SUSTAINABLE AQUACULTURE

Overall Project Development and Discharge Summary

Nordic Aquafarms Inc is planning to construct a land-based salmon farm in Belfast, Maine based on know-how and designs developed and implemented in Norway and Denmark. The facility value chain will include a hatchery that receives delivery of salmon eggs and spans the entire process with output of head-on gutted fish and filets. The hatchery will be subject to quarantine measures to ensure biosecurity. The facility will not include brood stock. Local planning and construction will be managed by our local US team and Maine construction partners, in partnership with our Norwegian engineering team.

Any fish farm will have a primary discharge of nutrients related to feed metabolism. In this case, feces, feed particles and dissolved nutrients will be key discharge factors to manage.
With scaling up of land-based farms, the need to employ environmental technologies increases. We are also of the opinion that this industry as a whole must raise its environmental standards in the years to come. Today, we see very few farms internationally that reduce nitrogen and phosphorous discharge because they have not had incentives to do so.

For this reason, Nordic Aquafarms has pursued significant development related to efficient discharge treatment. Nordic Aquafarms is employing tried and proven technologies to significantly reduce nutrients, including nitrogen and phosphorous. Our waste water treatment infrastructure involves investments to minimize local environmental impact. The joint conclusion from us and our US consultants, is that the residual discharge will have minimal environmental impact due to the high level of nutrient removal and the chosen discharge point off shore.

CORMIX and ADCIRC modelling has also been conducted by our US partner Ransom Consulting to evaluate potential impact in local waters, and to assess the best possible position for the discharge point. This modelling shows that the facility discharge will not impact eelgrass beds or other potential sensitive receptors. The modelling shows that the residual nutrients being discharged are sufficiently treated and diluted to be protective of Belfast Bay. See separate attachments for CORMIX and ADCIRC modeling.

With nutrient removal rates at 99 percent for many key discharge parameters, we are not familiar with any larger smolt or grow-out facilities that are even close to these removal rates. Our analysis of back-ground water quality parameters in the bay also show that our discharge of particles (TSS) is lower than existing values in the bay. In our experience, our removal rates are also higher than most other industries treating a discharge.

In conclusion, Nordic Aquafarms is applying state of the art technologies and standards that go well beyond current industry standards. Further discharge reductions are not feasible with current available technologies. Actual residual discharge figures are included in the application.

Memo

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Date:	September 27, 2018
To:	Nordic Aquafarms
From:	Nathan Dill, P.E.
Subject:	Near-field Dilution of Proposed Discharge

This memorandum provides a summary of estimated initial dilution of wastewater discharge from the proposed Nordic Aquafarms Recirculating Aquaculture System into Belfast Bay, Maine. This memorandum focuses on dilution of the effluent that would occur within the near-field region. That is, the region near the discharge port where mixing is dominated by forces of the discharge itself, and thus can be influenced by the outfall design.

Understanding the near-field dilution of a wastewater discharge is typically important when there is a need to assess impacts of toxic pollutants on aquatic organisms near the outfall. However, in this case, the proposed discharge for Nordic Aquafarms does not contain any toxic components, and there is no need to define a mixing zone. As such, the information in this memorandum is provided primarily to elucidate near-field mixing processes and aid in outfall design.

To aid in understanding near-field mixing process and outfall design, dilution has been evaluated for a variety of possible conditions, including a single-port or multi-port diffuser, and for a range of conditions representative of seasonal and tidal variations in ambient conditions. Dilution values and associated information provided in this memorandum are representative of the dilution that would occur within the plume after 15 minutes of travel time along the plume centerline from the point of discharge.

DILUTION MODELING WITH CORMIX

The Cornell Mixing Zone Expert system (CORMIX)[1] is a series of software subsystems for the analysis, prediction, and design of aqueous toxic or conventional discharges into diverse water bodies. CORMIX utilizes a rule-based, expert systems approach to determine the relative importance of various physical processes, and then applies the appropriate numerical modules to simulate mixing, dilution, and plume trajectory in both near-field and far-field regions. The result is a qualitative and quantitative description of the discharge as it evolves from a near-field jet dominated by effluent characteristics and port geometry to a far-field plume transported and

[1]Doneker, R.L. and G.H. Jirka. CORMIX1: An Expert System for Mixing Zone Analysis of Conventional and Toxic Single Port Aquatic Discharges. 1990, USEPA: Athens, GA.

dispersed by ambient conditions. The expert system methodology reduces the potential for user input error, resulting in a reliable system for jet/plume analysis. CORMIX is supported by the U.S. Environmental Protection Agency (USEPA) and is widely applied and accepted by the environmental community. CORMIX version 11.0 was used for the analysis documented in this report.

EFFLUENT AND DISCHARGE

CORMIX requires specification of various parameters that describe the physical characteristics of the effluent, as well as the geometry of the outfall and discharge port. The following effluent and discharge port characteristics have been assumed based on information provided by Nordic Aquafarms:

- Flow rate of 0.337 m^3/s (7.7 mgd)
- Effluent Density 1014.8 kg/m^3 (representative of a 2:1 mixture of seawater:freshwater at approximately 13 degrees C)
- Discharge port diameter 0.762 m (2.5 feet), or 0.381 m (1.25 feet)
- Discharge port oriented 20 degrees above horizontal, perpendicular to ambient flow direction 1.5 meter (5 feet) above bottom
- Alternative multi-port diffuser with three 0.3 meter (1 foot) diameter ports, spaced 15 m (50 feet) apart, oriented perpendicular to ambient flow. Discharge ports oriented 20 degrees above horizontal and perpendicular to ambient flow direction.
- Outfall located at depth of 8 meters, 500 meters from the shoreline; or depth of 15 meters, 1000 meters from the shoreline.

AMBIENT CONDITIONS

Ambient conditions have been characterized using information from available literature.[2,3,4] It is noteworthy that none of the available data used to approximate ambient tidal current velocity conditions were collected specifically in the area of the proposed discharge in Belfast Bay. Although an attempt has been made to use information that is relevant to the Belfast Bay region in northwestern Penobscot Bay, the available tidal current velocity data were collected in locations that generally farther offshore and in deeper water than the proposed discharge locations.

[2] Burgund, H.R. 1995. The Currents of Penobscot Bay, Maine, Observations and a Numerical Model. Senior thesis presented to the faculty of the Department of Geology and Geophysics, Yale University.
[3] Normandeau, 1978. An Oil Pollution Prevention Abatement & Management Study for Penobscot Bay, Maine. Volume II, Chapters 6-7. Prepared for the State of Maine Department of Environmental Protection Division of Oil Conveyance Services under Contract No. 907313.
[4] Fandel, C. L., T.C. Lippmann, J.D. Irish, L.I.Brothers. 2016. Observations of Pockmark Flow Structure in Belfast, Bat, Maine. Part 1: Current-induced Mixing. Geo-Mar Lett.

The following assumptions have been made to describe the depth averaged tidal current range and seasonal stratification at the proposed discharge location within Belfast Bay:

- Tidal currents of 0.05 m/s for slack tide, 0.2 m/s for flood and ebb tide.
- Ambient density stratification for winter, spring, summer, and fall seasons as illustrated in Figure 1 and Figure 2 for the deep and shallow discharge location, respectively.

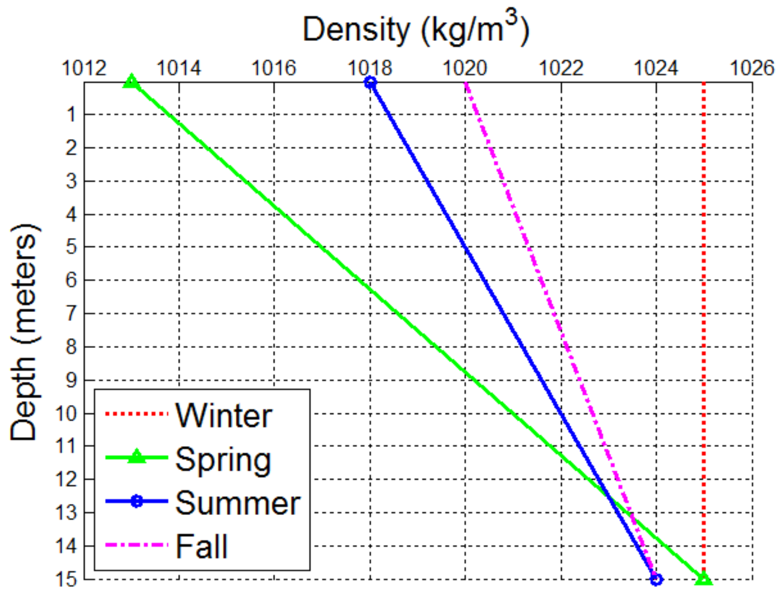

Figure 1. Assumed seasonal density profiles at deep discharge location

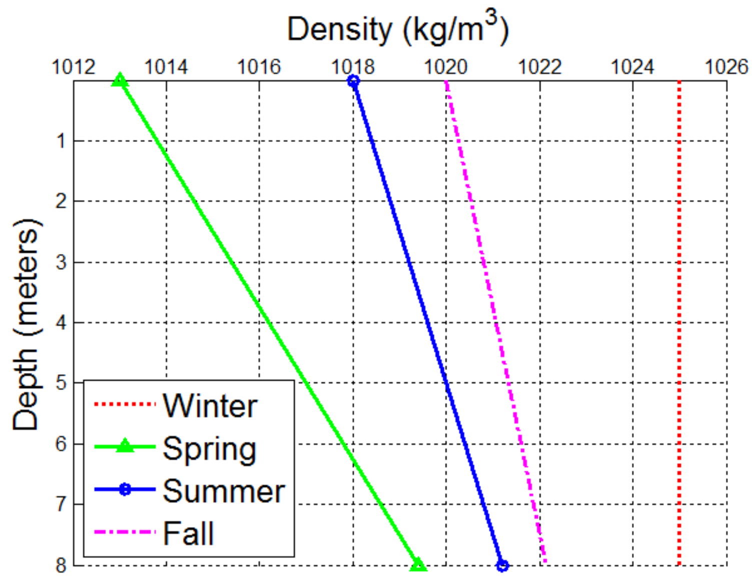

Figure 2. Assumed seasonal density profiles at shallow discharge location

RESULTS AND DISCUSSION

The range of ambient conditions and discharge locations results in a total of 32 unique CORMIX simulations for consideration with a single port discharge, or 16 unique simulations for the multi-port diffuser. The results describing the predicted CORMIX flow class and near-field dilution for the single port discharges are listed in Table 1. Results for the multiport diffuser are listed in Table 2. Important plume characteristics given in Table 1 and Table 2 include the distance from the discharge port at 15 minutes travel time[5], dilution at 15 minutes travel time, and the associated percent of initial concentration excess.

The dilution is the proportion of ambient water to effluent entrained in the plume. For example, if 1 liter of effluent is mixed with enough ambient water to make 10 liters of mixed water, the resulting dilution is 10. The percent initial concentration excess is related to the dilution by the following equation; it allows for easy estimation of the concentration of a specific wastewater constituents when the effluent concentration and background concentrations are known. For example, if the excess concentration (i.e. effluent concentration minus background concentration) is 100 mg/l, a 10% initial concentration excess would mean the concentration at the end of the near-field region is predicted to be 10 mg/l (above background).

$$C = Cs + \frac{1}{S}(Cd - Cs)$$

[5] This distance is calculated along the portion of the plume centerline downstream from the discharge port. where upstream intrusion is predicted the length of the plume may approach twice this distance. Upstream intrusion is generally predicted when the ambient current speed is low relative to the influence of buoyancy. This tends to occur during simulations representative of slack tide conditions.

Where *C* is the concentration corresponding to dilution, *S*. *Cs* is the background concentration, and *Cd* is the effluent concentration[6].

CORMIX input files, session reports and prediction files are available upon request.

Shallow Discharge Location

At the shallow discharge location CORMIX predicts the possibility of 3 different flow classifications for the range discharge and ambient configurations (classes H2, H4-90, and S3 for single port discharge, and MU6, MS1, MS4, and MU1V for the multi-port diffuser). It is likely that the discharge jet-plume will evolve through these different flow classes within the tidal cycle and throughout the seasons.

Shallow Single Port

For the single port discharge the H2 class occurs when the current speed is relatively high and discharge port is large, while the H4-90 class occurs for the smaller port size and at slack tides. In general, the "H" classes describe a jet/plume that is dominated by buoyancy in a relatively uniform ambient layer. This results in a plume that rises quickly after the discharge port and forms a layer at the water surface. For the H4-90 class, the plume may become attached to the bottom at times because the depth becomes relatively small when compared to the length of the initial jet, and the discharge is nearly horizontal. The S3 class, which describes a plume that becomes trapped below the surface within the ambient stratification, is only predicted during slack tides in the spring season when the stratification is strong, and currents are weak.

Shallow Multi-Port

The MU6 flow class is predicted for the multi-port diffuser at the shallow discharge location during the winter season for both slow and fast current speed. MU6 is also predicted during spring, summer, and fall when the current speed is low. MU6 describes a plume that becomes vertically mixed throughout the water column within the near field region as turbulence from the discharge jet dominates the relative unimportance of the stratification. In contrast, "MS" classes are predicted with stratification dominates resulting in buoyant plume that quickly rises after the point of discharge and becomes trapped below the surface within the ambient stratification. This occurs for both current speeds during the spring, and when currents are faster in the summer and fall. The MS4 class, which occurs in spring during slow currents, differs from the MS1 class in that significant upstream intrusion of the plume may occur. During the summer and fall when the current is faster, upstream intrusion of the trapped plume is prevented by the speed of the current.

Deep Discharge Location

Deep Single Port

At the deep discharge location CORMIX predicts the possibility of 6 flow classes (H1, H2, H4-90, S1, S3, S4, and S5). In general, the "H" classes describe a jet/plume that is dominated by

[6] Fischer, H.B., E.J. List, R.C.Y. Koh, J.Imberger, N.H.Brooks,. 1979. Mixing in Inland and Coastal Waters. Academic Press Inc., New York, NY. 483 p.

buoyancy in a relatively uniform ambient layer. This results in a plume that rises quickly after the discharge port and forms a layer at the water surface. At the deep discharge location these conditions primarily occur during the winter season when there is no stratification, and in the fall when stratification is weak and the smaller discharge port is used. In general, “S” classes describe a near-bottom discharge of buoyant plume that becomes trapped in the ambient stratification. The behavior can be qualitatively described by considering that a less dense effluent discharged into the ambient water will entrain ambient water lowering the density of the plume while it rises in the water column until it forms a stable layer where the density of the ambient water above the layer is less than the density of the plume. More detail of the behavior is elucidated by considering whether the plume is more jet like or plume like, and whether the ambient current dominates the jet/plume. In the S1 or S3 class the plume has a more jet like behavior, while S4 or S5 indicate a more plume like behavior. The more jet like conditions occur with the smaller port diameter, which tends to increase the dilution. The S1 or S4 classes occur when currents are stronger during flood or ebb tides indicating that the plume will be strongly deflected increasing dilution. The S3 or S5 classes occur during slack tide when some buoyant upstream intrusion of the plume is expected, tending to reduce dilution somewhat.

Deep Multi-Port

In general buoyancy is more important at the deep discharge location and plume behavior will be more stable because of the greater depth. When current speeds are fast during flooding or ebbing tides the deep multi-port diffuser is plume is classified the same as it is for the shallow discharge location. That is, a fully vertically mixed near-field plume during winter, and a trapped buoyant plume in the spring, summer, and fall seasons that is strongly deflected by the ambient current. When current speeds are low significant upstream intrusion is predicted. During slack tides in winter the plume is predicted to rise to the surface and intrude upstream (MU1V), while during slack tides in the other seasons the upstream intruding plume is expected to become trapped within the ambient stratification.

Table 1. CORMIX Results for Single Port Discharge at 15 minutes Travel Time

Location	Current (m/s)	Season	Port Diameter (m)	CORMIX Flow Class	Distance From Port* (m)	Dilution	% Initial Conc. Excess
Shallow	0.2	Winter	0.761	H2	182.2	51.5	2.0
Shallow	0.2	Winter	0.381	H4-90	183.9	51.1	2.0
Shallow	0.2	Spring	0.761	H2	182.0	73.5	1.4
Shallow	0.2	Spring	0.381	H4-90	185.9	83.0	1.2
Shallow	0.2	Summer	0.761	H2	182.6	60.7	1.7
Shallow	0.2	Summer	0.381	H4-90	187.9	72.8	1.4
Shallow	0.2	Fall	0.761	H2	182.6	60.2	1.7
Shallow	0.2	Fall	0.381	H4-90	184.8	56.9	1.8
Shallow	0.05	Winter	0.761	H4-90	46.3	7.7	13.0
Shallow	0.05	Winter	0.381	H4-90	83.9	48.7	2.1
Shallow	0.05	Spring	0.761	S3	47.5	7.3	13.9
Shallow	0.05	Spring	0.381	S3	48.7	14.8	6.8
Shallow	0.05	Summer	0.761	H4-90	66.3	24.1	4.2
Shallow	0.05	Summer	0.381	H4-90	82.6	32.8	3.0
Shallow	0.05	Fall	0.761	H4-90	46.5	7.2	13.9
Shallow	0.05	Fall	0.381	H4-90	83.6	38.7	2.6
Deep	0.2	Winter	0.761	H1	186.1	96.9	1.0
Deep	0.2	Winter	0.381	H2	187.0	116.4	0.9
Deep	0.2	Spring	0.761	S4	182.3	47.4	2.1
Deep	0.2	Spring	0.381	S1	184.8	79.6	1.3
Deep	0.2	Summer	0.761	S4	183.3	58.8	1.7
Deep	0.2	Summer	0.381	S1	186.1	97.3	1.0
Deep	0.2	Fall	0.761	S4	184.2	68.4	1.5
Deep	0.2	Fall	0.381	H2	187.4	106.8	0.9
Deep	0.05	Winter	0.761	H4-90	48.8	16.4	6.1
Deep	0.05	Winter	0.381	H4-90	91.3	104.9	1.0
Deep	0.05	Spring	0.761	S5	47.5	9.3	10.8
Deep	0.05	Spring	0.381	S3	49.1	16.4	6.1
Deep	0.05	Summer	0.761	S5	48.6	13.0	7.8
Deep	0.05	Summer	0.381	S3	50.9	20.6	4.9
Deep	0.05	Fall	0.761	S5	48.6	12.6	8.0
Deep	0.05	Fall	0.381	S3	52.2	24.0	4.2

*straight line distance to plume centerline at 15 minutes travel time from port. In some cases, the plume may be significantly wider than this distance and may include upstream intrusion.

Table 2. Summary of CORMIX Results for Diffuser at 15 minutes Travel Time

Location	Current (m/s)	Season	CORMIX Flow Class	Distance From Port* (m)	Dilution	% Initial Conc. Excess
Shallow	0.2	Winter	MU6	180.2	212.2	0.5
Shallow	0.2	Spring	MS1	190.5	50.3	2.0
Shallow	0.2	Summer	MS1	194.7	66.8	1.5
Shallow	0.2	Fall	MS1	197.6	80.9	1.2
Shallow	0.05	Winter	MU6	47.5	43.9	2.3
Shallow	0.05	Spring	MS4	53.5	13.5	7.5
Shallow	0.05	Summer	MU6	47.5	43.6	2.3
Shallow	0.05	Fall	MU6	47.5	43.7	2.3
Deep	0.2	Winter	MU6	180.6	350.1	0.3
Deep	0.2	Spring	MS1	192.2	56.9	1.8
Deep	0.2	Summer	MS1	195.5	72.1	1.4
Deep	0.2	Fall	MS1	197.8	84.3	1.2
Deep	0.05	Winter	MU1V	69.2	61.5	1.6
Deep	0.05	Spring	MS4	55.1	17.5	5.7
Deep	0.05	Summer	MS4	55.8	19.3	5.2
Deep	0.05	Fall	MS4	58.1	24.0	4.2

RECOMMENDATIONS

- In general, the results indicate that a reduced port size will lead to higher outlet velocity and increased initial dilution. It is recommended that the smaller port size be considered in design of the outfall, for either the single port or multi-port diffuser.

- The multi-port diffuser yields similar initial dilution as the single port with smaller outlet diameter. However, the behavior of the multi-port diffuser is more consistent at the different depths in terms of CORMIX flow classifications. This suggests the plume behavior from a multi-port diffuser may be less sensitive to the outfall location.

- The results presented here assume the discharge is occurring at full capacity. Discharge at a reduced rate at facility start up may require design modifications to achieve similar initial dilution at reduced discharge rates. The use of duckbill type check valves on the outfall ports may be considered to help maintain outlet velocities under a range of discharge flow rates. Furthermore, the use of a multi-port diffuser may facilitate a scaling up of the discharge flow rate as ports may be initially closed and then opened in sequence as the discharge capacity is increased.

- Site specific ambient conditions data should be collected during facility operations to evaluate whether observations are significantly different than model assumptions and predictions.

- The application of the CORMIX model in tidal environments is limited by an assumption of steady-state conditions. This precludes the ability of CORMIX to estimate long term dilution when it is possible for reversing tidal currents to recirculate the plume past the discharge location. Evaluation of the 2-dimensional far-field behavior of the plume and the potential for recirculation of discharged water and build up of effluent in the receiving water body is discussed in an additional memo that accompanies the Maine Pollutant Discharge Elimination System (MEPDES) Permit Application.